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## Post Breakage Strength Testing for Overhead Laminated Glass

I. Stelzer <sup>a</sup> & M. Singh Rooprai <sup>b</sup> <sup>a</sup> Kuraray Europe GmbH, Germany, ingo.stelzer@kuraray.com <sup>b</sup> Kuraray India

Design and structural performance of laminated glass in over-head glazing applications like canopies, skylights is very critical as it has an impact on the safety of occupants of a building and its maintenance workers. For such applications post breakage strength of laminated glass construction is of utmost importance. Pre breakage strength can be predicted with reasonable accuracy by FEM technique based software packages, which allow the user to input mechanical properties of viscoelastic interlayers along with glass. This helps in interlayer based differentiation of pre breakage structural strength and design optimization. However, post breakage structive testing is the only reliable solution. Impact testing, simulating the accidental fall of a maintenance worker was done to assess the "fall through" resistance of point fixed laminated glass constructions having varying interlayers viz, PVB, Ionoplast Interlayer, Stiff PVB, and EVA. In addition, medium duration (30 mins or more ) post breakage strength tests driven by the new requirements set in place by German Standard pr DIN 18008-6 were conducted at subzero (-20°C), room temperature (+21°C) and at elevated temperatures of +50° Celsius.

Keywords: Laminated glass, post glass breakage, overhead, interlayer, PVB, EVA, Ionoplast,

#### 1. Introduction

Laminated glass has a significant improvement in the post breakage strength over a monolithic layer of glass, the glass fragments adhere to the interlayers so that a certain remaining structural capacity is obtained as the glass fragments 'arch' or lock in place. This capacity depends on the fragmentation of the glass and increases with increasing fragment size. Therefore, laminated glass elements would typically achieve a particularly high remaining structural capacity when made from annealed or heat strengthened glass that breaks into large fragments. The post breakage behavior furthermore depends on the interlayer material. The most common interlayer is PVB whose mechanical properties are heavily depended on temperature and load duration. At room temperature, PVB is soft with an elongation at break of more than 250%. For higher temperatures and load durations the shear transfer is greatly affected. Low stiffness of the PVB interlayer results in "Wet Blanket Effect" (Fig. 1) as soon as the glass breaks even for vertical applications because of the self-weight of the panel especially with large panel sizes and minimal supports. SentryGlas® lonoplast Interlayer, from Kuraray (originally invented by DuPont), was developed with the aim of achieving higher stiffness, temperature resistance, resistance to tearing in point fixed rotule applications. This helps in achieving a superior post breakage strength and design redundancy.



Fig.1 The "Wet Blanket" Effect

CG<sup>©</sup> Challenging Glass 5 Table 1: Comparison of Mechanical Properties of SentryGlas<sup>®</sup> and Standard PVB

Interlayer Type	Density	Young's Modulus @ 50°C, for 1 hour load	Poisson Ratio	Coefficient of Thermal Expansion	Tensile Strength
SentryGlas® Ionoplast	850 kg/m <sup>2</sup>	12.6 MPa	0.5	12.5 x 10 <sup>-5 / °C</sup>	34.5 MPa
Standard PVB (Butacite®)	1070 kg/m <sup>3</sup>	0.16 MPa	0.5	$2.2 \ x \ 10^{-4} / ^{\circ C}$	20 MPa

Above table gives a comparison of the mechanical properties of SentryGlas® Ionoplast and Standard PVB interlayers. Post breakage strength is significantly affected by the breakage pattern of the glass layers, support conditions, and temperature. Breakage pattern of glass can be a big variable even for the same type of glass and this makes analytical modeling of its post breakage strength a near impossible task. Thus engineers have to rely on destructive testing for this. Post breakage strength can be categorized as follows.

Immediate Post Breakage Strength against "fall through"

Medium Duration Post Breakage Strength Testing (More than 30 Mins. As per pr DIN 18008 - 61)

Separate tests were conducted for both above types of strengths and same have been presented in this paper.

#### 2. Post Breakage Strength Testing

#### 2.1. Immediate Post Breakage Strength against "Fall Through"

Impact tests were done at Intertek ATI Inc. York, Pennsylvania by dropping a soft bag weighing 100 Kg (typical weight of maintenance working carrying his tools and personal equipment) from a height of 1200 mm at a test temperature of 50°C. The test method simulates potential loading from installation and /or maintenance workers in distress. The panels were conditioned at 50°C for 1 hour before the test. The test set up was enclosed with insulated panels and the temperature controlled by an air conditioning device to ensure there is no variation in test results due to temperature. The insulated panels on top of the glass were were removed just before the impact (Fig. 2).

Table 2. Glazing Constructions							
Dimension of the Specimen: 1.194 mm x 1.500 mm							
Supports: Rotule System CR-Laurence (fully motion restricted)							
Laminate Construction 1.	Laminate Construction 2.	Laminate Construction 3.	Laminate Construction 4. & 5.				
2 x 6 mm FT-Glass	2 x 6 mm FT-Glass	2 x 6 mm FT-Glass	2 x 6 mm FT-Glass				
1.52 mm Interlayer	1.52 mm Interlayer	1.52 mm Interlayer	0.89 mm / 1.52 mm Interlayer				
Butacite® PVB	Low plasticizer PVB (DG41)	EVAsafe®	SentryGlas®				
"Standard PVB"	"Stiff PVB"	"EVA"	"Ionomer"				

Fig. 3 shows how the laminate made from SentryGlas® Ionoplast Interlayer provided a barrier against the impactor. The impactor was removed after 15minutes without any tearing of interlayer observed at the rotules. Whereas laminates made from EVA, Standard PVB and Stiff PVB in Fig. 2, 3, 4, 5, 6 respectively, collapsed as soon as the impactor strikes, and failed to act as a barrier.



Fig. 2 (a & b) Impact Test on a Frameless (point supported) canopy application, view from above showing the impactor before the impact (a) and a close-up picture of the rotule type fixation system



Fig. 3 Ionomer laminate provided "Fall Through" resistance, view from below during the impact

Fig. 4 EVA laminate provided no "Fall Through" resistance, view from below just after the impact, see failure of the laminate



Fig. 5 Standard PVB laminate provided no "Fall Through" resistance, view from below just after the impact, see failure of the laminate

Fig. 6 Stiff PVB laminate provided no "Fall Through" resistance view from below just after the impact, see failure of the laminate

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# 2.2. Medium Duration Post Breakage Strength Testing (30 Minutes or more) Standards Requirement<sup>1</sup>

German Standard pr DIN 18008 – 61, (Glass in Buildings – Design & Construction Rules – Additional requirements for walk-on glazings in case of maintenance procedures) in February 2015, has made the post breakage performance requirements for an overhead glazing, that is accessible for maintenance and cleaning, much more stringent than ever before. The new regulation requires a laminated glass construction to sustain the weight of 100 Kg for at least 30 minutes after breakage of top layer of glass. First, the panel is subjected to an impact made by dropping a twin tyre impactor which weights 50Kg from a height of 900 mm. This is followed by imposing a load of 100 Kg for 30 minutes on an area of 200 x 200mm. After breakage of the uppermost glass layer, the whole glazing element must stay on its supports for at least 30 minutes. The test is successful if the specimen does not slide from the supports, the impact does not penetrate the laminated glass and no dangerous glass fragments fall down2.



Fig. 7 Post Breakage Test layout in climate chamber

Post breakage strength tests on point supported glass panels (1500 mm x 2000 mm) for a typical canopy application were conducted at University of Armed Forces in Munich, Germany. 9 glass panels with each of 4 different interlayers – Ionomer (1.52 & 0.89mm), Stiff PVB (1.52mm) , and PVB (1.52 mm) were prepared for testing at 3 different temperature scenarios.

Table 3. Glazing Constructions							
Dimension of the Specimen: 1.500 mm x 2.000 mm							
Supports: PAULI & SOHN Rotule System 751260 VAM 16 (not fully motion restricted)							
Laminate Construction 1.	Laminate Construction 2.	Laminate Construction 3.	Laminate Construction 4.				
2 x 6 mm FT-Glass	2 x 6 mm FT-Glass	2 x 6 mm FT-Glass	2 x 6 mm FT-Glass				
1.52 mm Interlayer	1.52 mm Interlayer	0.89 mm Interlayer	1.52 mm Interlayer				
Butacite® PVB	Trosifol® EXTRA STRONG	SentryGlas®	SentryGlas®				
"Standard PVB"	"Stiff PVB"	"Ionomer"	"Ionomer"				

#### Post Breakage Strength Testing for Overhead Laminated Glass

The objective was to know which interlayer type laminate construction can pass the requirements set by pr DIN 18008-6 at 3 different temperatures ( $-20^{\circ}C$ ,  $+21^{\circ}C$  and  $+50^{\circ}C$ ). 3 panels were tested for each temperature scenario. An attempt was made to know the ultimate capacity of the laminates. However, the test apparatus had a limitation of applying a maximum load of 400 Kg. The laminates were conditioned for at least 3 hours for each temperature scenario. The test chamber had a temperature control mechanism (AC-System) for a temperature range of  $-25^{\circ}C$  to  $+50^{\circ}C$ . The laminate construction with all different types of interlayers was strong enough to withstand the impact against any breakage. Therefore the upper layer of laminates in each case had to be broken manually with a centre punch. It was followed by placing a 100 Kg concrete block on the glass panel for 30 minutes. The test was aimed to know the ultimate post breakage performance limit so load was ramped up to 400 Kg in increments of 100 Kg, with a 15 minute time interval between each load increment.

Laminates with Ionomer and Stiff PVB interlayers sustained this load of 400 Kg without collapse at -20 °C and + 21°C temperatures (Fig. 11) Whereas in Fig. 9, Standard PVB laminate could not sustain the 100 Kg imposed load at +21°C as it collapsed in few seconds when load was placed due to tearing of the interlayer at the rotules.



Fig. 8 400Kg load on Ionomer laminate at +21°C

Fig. 9 Collapsed PVB laminate with 100Kg at +21°C

At elevated temperature of 50°C, broken laminate construction with PVB & Stiff PVB interlayers could not sustain their own self weight as they collapsed (Fig. 10 & Fig. 12) soon after breakage of both layers.



Fig. 10 Broken Standard PVB laminate collapsed at +50°C



Fig. 11 Broken Stiff PVB laminate collapsed at +50°C

Whereas, the laminate construction made with 0.89 mm Ionomer interlayer sustained a weight of 100 Kg for more than 30 minutes and collapsed when load was ramped up to 200 Kg. (Fig. 12). Similarly, 1.52 mm Ionomer laminate could sustain a load of 200 Kg for more than 30 minutes after breakage and collapsed when load was ramped up to 300 Kg (Fig. 13).

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Fig. 12 0.89mm Ionomer laminate collapsed at 200Kg at +50°C



Fig. 13 1.52mm Ionomer laminate collapsed at 300Kg at +50°C

#### 3. Deflection Measurements for Estimating Modulus of Broken Laminate

Deflection measurements were made during the test for all three temperature scenarios to make an estimate of the post glass breakage strength of the laminate constructions. At -20 °C the 1.52 mm Ionomer laminate demonstrated the lowest deflection after 30 min (Fig. 17), whilst at +21°C both Ionomer laminates (1.52 and 0.89 mm) outperformed the PVB laminates (Fig. 18).



Fig. 14 Deflection Vs Time Measurements @ -20°C Butacite® = Standard PVB, Trosifol® ES = Stiff PVB, SentryGlas® = Ionomer

Post Breakage Strength Testing for Overhead Laminated Glass



Fig. 15 Deflection Vs Time Measurements @ +20°C Butacite® = Standard PVB, Trosifol® ES = Stiff PVB, SentryGlas® = Ionomer

#### 4. Conclusions

- At -20°C, laminates made from the 4 interlayer candidates i.e 0.89 mmIonomer, 1.52 mm Ionomer, mm Standard PVB, 1.52 Stiff PVB pass the post breakage strength requirements of the new German Standard pr DIN 18008 6.
- At -20°C, all 4 candidates had their ultimate strength more than 400 Kg as there was no collapse of the panel due to tearing of the interlayer at rotules.
- At +21°C, Ionomer and Stiff PVB laminates pass the post breakage strength requirements of DIN 18008 6 but Standard PVB laminate does not (for this type of construction).
- At +21°C, 0.89 mm & 1.52mm Ionomer laminate had almost similar post breakage strength till about 45 minutes from the breakage.
- For tropical climate regions where the ambient temperature is more than +45°C, Ionomer interlayer laminates meet and exceed the requirements of pr DIN 18008- 6 Standard.
- Further testing and research will be conducted to get a better understanding of the post glass breakage behavior of laminated glass and to develop appropriate design methods.

#### References

Draft Standard / DIN prEN 18008-6, Beuth-Verlag, Berlin GS-BAU-18, Merkblatt ZiE-Nr. 3A

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